Chartes's Law
$\mathrm{T} 1 \times \mathrm{V} 2=\mathrm{T} 2 \mathrm{~V} 1$
or
$\mathrm{T} 1 \times \mathrm{P} 2=\mathrm{T} 2 \mathrm{P} 1$


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## Understanding Circuit Symbols

Directional air control valves are the building blocks of pneumatic control. Symbols representing these valves provide a wealth of information about the valve it represents. Symbols show the methods of actuation, the number of positions, the flow paths and the number of ports. Here is a brief breakdown of how to read a symbol:

Every symbol has three parts (see figure to right). The Left and Right Actuators are the pieces which cause the valve to shift from one position to another. The Position and Flow Boxes indicate how the valve functions. Every valve has at least two positions and each position has one or more flow paths.

When the Lever is not activated, the Spring Actuator (right side) is in control of the valve; the box next to the actuator is the current
 flow path. When the Lever is actuated, the box next to the Lever is in control of the valve. Each position occurs when the attached actuator is in control of the valve (Box next to the actuator). A valve can only be in one "Position" at a given time.

The number of boxes that makes up a valve symbol indicates the number positions the valve has. Flow is indicated by the arrows in each box. These arrows represent the flow paths the valve has when it is that position (depending upon which actuator has control over the valve at that time).

The number of ports is determined by the number of end points in a given box (only count in one box per symbol as the other boxes are the just showing different states of the same valve). In the example, there are a total of 5 ports. NOTE: Sometimes a port (such as exhaust) goes directly to atmosphere and there is no port to attach to. To spot this, the actual ports line will extend beyond the box, while the ports you cannot attach to will not.
 A Port is blocked with this symbol: $\mathbf{T}$
Following is a list of symbols and what they mean:

Valve Symbols, Flow Paths and Ports


2-Position, 2-Way, 2-Ported

2-Position, 3-Way, 3-Ported

2-Position, 4-Way, 4-Ported


2-Position, 4-Way, 5-Ported


3-Position, 4-Way, 4-Ported Closed Center

Actuator Symbols
 Q Mechanical

Spring


Detent

Solenoid

Actuator Symbols
Lines

--D External Pilot


Piloted Solenoid with Manual Override

$\perp \xrightarrow{\perp}$ Lines Joined


Lever Operated, Spring Return


Solenoid Operated, Spring Return

## Simple Pneumatic Valves

Flow Control, 1 Direction


Relief Valve

## $C_{v}$ Defined



Q: What does " $\mathrm{C}_{\mathrm{V}}$ " mean?
A: Literally $\mathrm{C}_{\mathrm{V}}$ means coefficient of velocity. $\mathrm{C}_{\mathrm{V}}$ is generally used to compare flows of valves. The higher the $C_{V}$, the greater the flow.

It is sometimes helpful to convert $\mathrm{C}_{\mathrm{V}}$ into SCFM(Standard Cubic Feet per Minute) and conversely, SCFM into $C_{V}$. Although $C_{V}$ represents flow capacity at all pressures, SCFM represents flow at a specific air pressure. Therefore, the following chart relates $\mathrm{C}_{\mathrm{V}}$ to SCFM at a group of pressures.
To obtain SCFM output at a particular pressure, divide the valve $\mathrm{C}_{\mathrm{V}}$ by the appropriate factor shown below.

| Cv to SCFM Conversion Factor Table |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PSI of Air Pressure | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| Factor | .0370 | .0312 | .0270 | .0238 | .0212 | .0192 | .0177 |

Example: What is the output in SCFM of a value with a $C_{V}$ of 0.48 when operated at 100 PSI ? $\frac{0.48(C V)}{.0177 \text { (Factor) }}=27$ SCFM $\begin{aligned} & \text { To convert SCFM into } C_{V} \text {, simply reverse the process and multiply } \\ & \text { the SCFM times the factor }\end{aligned}$

## Pneumatic Valve Sizing

Two methods are shown below to aid in the selction of a pneumatic valve. To account for various losses in all pneumatic systems, remember to over-szie by at least $25 \%$.

## Method 1: Calculation

This formula and chart will give the $\mathrm{C}_{V}$ (Valve flow) required for operating a given air cylinder at a specific time period.

$$
\mathrm{C}_{V}=\frac{\text { Area } \times \text { Stroke } \times \mathrm{A} \times \mathrm{C}_{f}}{\text { Time } \times 29}
$$

Area $=\pi \times$ Radius 2 or see table $B$ below.
Stroke = Cylinder Travel (in.)
A = Pressure Drop Constant (see table A) $C_{f}=$ Compression Factor (see table A)
Time $=\ln$ Seconds
Table A

| Inlet <br> Pressure <br> (PSI) | Compres <br> sion <br> Factor | "A" Constants for Various <br> Pressure Drops |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 2 PSI <br> $\Delta \mathrm{P}$ | 5 PSI <br> $\Delta \mathrm{P}$ | 10 PSI <br> $\Delta \mathrm{P}$ |  |
| 10 | 1.6 |  | 0.102 |  |
| 20 | 2.3 | 0.129 | 0.083 | 0.066 |
| 30 | 3.0 | 0.113 | 0.072 | 0.055 |
| 40 | 3.7 | 0.097 | 0.064 | 0.048 |
| 50 | 4.4 | 0.091 | 0.059 | 0.043 |
| 60 | 5.1 | 0.084 | 0.054 | 0.040 |
| 70 | 5.7 | 0.079 | 0.050 | 0.037 |
| 80 | 6.4 | 0.075 | 0.048 | 0.035 |
| 90 | 7.1 | 0.071 | 0.045 | 0.033 |
| 100 | 7.8 | 0.068 | 0.043 | 0.031 |
| 110 | 8.5 | 0.065 | 0.041 | 0.030 |
| 120 | 9.2 | 0.062 | 0.039 | 0.029 |


| Bore Size | Cylinder <br> Area <br> (Sq. In.) |
| :---: | :---: |
| 1/4" | 0.049 |
| 1/2" | 0.196 |
| 3/4" | 0.44 |
| 1-1/8" | 0.99 |
| 1-1/2" | 1.77 |
| 2" | 3.14 |
| 2-1/4" | 3.97 |
| 2-1/2" | 4.91 |
| 3" | 7.07 |
| 3-1/4" | 8.30 |
| $4{ }^{\prime \prime}$ | 12.57 |
| $5{ }^{\prime \prime}$ | 19.64 |
| $6 "$ | 28.27 |
| 8" | 50.27 |
| 10" | 78.54 |
| 12" | 113.10 |

NOTE: Use " A " Constant at $5 \mathrm{PSI} \triangle \mathrm{P}$ for most applications.
For critical applications use " $A$ " at 2 PSI $\Delta P$. A 10 PSI $\Delta P$ will save money and mounting space.

## Method 2: Chart

Index $\mathrm{C}_{\mathrm{v}}$ against Bore Size vs. Inches of stroke per second.
Assuming 80 PSI and $\Delta \mathrm{P}=80 \%$.

| $\mathrm{C}_{v}$ | Cylinder Bore Size |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.75 | 1.13 | 1.50 | 2.00 | 2.50 | 3.25 | 4.00 | 5.00 | 6.00 | 8.00 |  |
| 0.1 | 26.8 | 11.9 | 6.7 | 3.8 | 2.4 | 1.4 | 0.94 | 0.6 | 0.42 | 0.24 |  |
| 0.2 | 53.7 | 23.9 | 13.4 | 7.5 | 4.8 | 2.9 | 1.9 | 1.2 | 0.84 | 0.47 |  |
| 0.5 | 134 | 59.6 | 33.6 | 18.9 | 12.1 | 7.1 | 4.7 | 3 | 2.1 | 1.2 |  |
| 1.0 | 268 | 119 | 67.1 | 37.7 | 24.2 | 14.3 | 9.4 | 6 | 4.2 | 2.4 |  |
| 2.0 | 537 | 239 | 134 | 75.5 | 48.3 | 28.6 | 18.9 | 12.1 | 8.4 | 4.7 |  |
| 4.0 |  | 477 | 268 | 151 | 96.6 | 57.2 | 37.7 | 24.2 | 16.8 | 9.4 |  |
| 8.0 |  |  | 536 | 302 | 193 | 114 | 75.5 | 48.3 | 33.6 | 18.9 |  |
| 16.0 |  |  |  | 604 | 387 | 229 | 151 | 96.6 | 67.1 | 37.7 |  |
| 32.0 |  |  |  |  | 773 | 457 | 302 | 193 | 134 | 75.5 |  |

## Valve Selection

Q: How do I select the right valve to control a cylinder?


A: There are many factors that contribute to the performance of a cylinder. Some of these factors are: quantity and type of fittings leading to the cylinder, tube length and capacity, cylinder operating load, and air pressure.

Rather than attempting to place a value on these, and other contributing factors, it is more practical to provide valve users with a general guide to valve sizing.

The sizing table below relates various air valves to cylinder bore sizes between $3 / /^{\prime \prime}$ and $6^{\prime \prime}$. The cylinder operating speed resulting from the use of each valve at 80 PSI is rated in general terms as:
" ${ }^{\prime \prime}$ " for High Speed Operation " $\mathbf{M "}^{\prime \prime}$ for Average Speed Operation " $\mathbf{S "}^{\prime}$ for Slow Speed Operation

| Valve Type | Cv | $\begin{aligned} & \text { Cyl. } \\ & \text { Type* } \end{aligned}$ | Cylinder Bore Sizes (in inches) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $3 / 4$ | 1 | $1^{1 / 8}$ | $1^{1 / 2}$ | 2 | $2^{1 / 4}$ | $2^{1 / 2}$ | 3 | $3^{1 / 4}$ | 4 | 6 |
| Micro-Line | 0.11 | SA |  | F |  |  |  | S |  | S |  |  |  |
| LTV | 0.18 | SA,DA | F | F | F | F | M | M | M | M | S | S |  |
| Nova | 1.00 | SA,DA |  |  | F | F | F | F | F | F | F | M | M |
| Duramatic | 0.18 | SA,DA | F | F | F | F | M | M | M | M | S | S |  |
| Duramatic | 0.63 | SA,DA |  |  | F | F | F | F | F | M | M | M | M |
| Capsula | 0.75 | SA,DA |  |  | F | F | F | F | F | F | M | M | M |
| Capsula | 3.17 | SA,DA |  |  |  |  |  |  |  |  | F | F | F |
| FT-1, FC-1 | 0.13 | SA |  | F |  |  |  | F |  | M |  | S |  |
| 4B-1, 4W-1 | 0.48 | SA,DA |  |  | F | F | F | F | M | M | M | S |  |
| FC51, PC51 | 0.81 | SA |  |  |  |  |  | F |  | F |  | M | M |
| FT-101, 201 | 1.15 | SA |  |  |  |  |  | F |  | F |  | F | F |
| Isonic V1 | 0.01-0.05 | SA | F | M |  |  |  |  |  |  |  |  |  |
| Isonic V4 | 0.8 | SA,DA |  |  | F | F | F | F | F | F | M | M | M |
| Isonic V3 | 0.03-0.11 | SA | F | F | F | M | S |  |  |  |  |  |  |
| Isonic V5 | 0.8 | SA,DA |  |  | F | F | F | F | F | F | M | M |  |

* SA = Single-Acting Cylinder, DA = Double-Acting Cylinder

Where no rating is shown, the valve is considered unsuitable for use with that particular bore size. To determine the suitability of valves not listed in the table, compare the $C_{V}$ of the unlisted valve with the one nearest it on the table and use that line for reference.

## SCFM Defined

Q: What does SCFM mean?
A: SCFM means Standard Cubic Feet per Minute. "Standard" is air at sea level and at $70^{\circ} \mathrm{F}$.

## Shuttle Valves

Q: Is there a valve that will direct air coming from either of two sources to a single destination?
A: Use a shuttle valve.


## Stacking



Q: How may I reduce piping and simplify trouble-shooting when a group of valves is used in an application?
A: Order your valves stacked to take advantage of a common air inlet, common exhausts, and control centralization.

## Time Delay



Q: Are there valves that allow me to delay a signal in my air circuit?
A: Yes, air timers can be used to delay an air signal. Up to 2 minute normally open or normally closed models are available.

## Two-Position - vs - Three-Position

Q: What is the difference between 2-position and 3-position valves?
A: In two-position four-way directional valves, the two output ports are always in an opposite mode. When one is receiving inlet air, the other is connected to the exhaust port.


When actuated, 3-position 4-way directional valves function the same as above. However, a center or "neutral" position is provided that blocks all ports (pressure held), or connects both output ports to the exhausts (pressure released) when the valve is not being actuated.

Pressure Held 3-Position Valves


Pressure held models are ideal for "inching" operations where you want the cylinder rod to move to a desired position and then hold.

## Pressure Released 3-Position Valves



## Five-Ported Valves

Q: What are the advantages of a five-ported four-way valve over a four ported four-way valve?
A: Five ported valves have separate exhaust ports for each cylinder port. If exhaust silencers with built-in speed controls are used, the speed of the cylinder motion may be individually controlled in each direction.


Also, five ported valves can function as dual pressure valves where air flows from the exhaust ports to the cylinder and both cylinder ports use the inlet as a common exhaust. Vacuum may also be used in five ported valves. Both the Nova line and the Capsula line provide five ported flow patterns.


## Flow Control



Q: Are there valves available that provide adjustable control of air flow?
A: Dylatrol valves perform this function. Also see the "Cylinders; Speed Control" question for application information. Dura-matic directional valves have built-in flow controls. Exhaust silencers typically have built-in needle valves that also provide speed regulation.

## Flow Patterns, 3-Way \& 4-Way

Q: What is the difference between a 3-way and a 4 -way valve?
A: Three-way valves have one power output and four-way valves have two power outputs.
Generally, three-way valves operate single-acting cylinders and four-way valves operate dou-ble-acting cylinders.

Three-Way Flow Pattern (Normally Closed)


Four-Way Flow Pattern (Two Position)


## For Safer Hand Actuation



Q: How may I keep the hands of my employees out of hazardous locations?
A: Use two-hand, anti-tiedown devices.

## Air -vs- Solenoid Actuation

Q: What are the advantages of air actuation over solenoid actuation?
A: Solenoid actuation requires the presence of electric switches, wires, and all of the shielding necessary to reduce spark hazard and personal risk.


NOTE: The Solenoid Valve shown here is N2-DCD.

Air actuation requires only 3 -way air pilot valves and tubing. There is no explosion, spark, or shock risk and the components are less expensive to buy.


## Detented Valves

Q: What is a "detented" valve and how is it used?
A: A detented valve is one that holds its position by some mechanical means such as a spring, ball or cam. Most valves hold their position by means of the natural friction of the rubber seals. Where natural friction is low, such as in packless valves, or where it is not enough for safety purposes, detented models are recommended. Also, detents are used to locate the middle position in three position valves.

## Air-To-Electric Signal Conversion

Q: Is it possible to convert an air signal into an electrical signal?
A: air-to-electric switches, MPE-BZ or MPE-BZE (includes enclosure), will turn an air signal into an electrical signal, which can be wired either normally open or closed.


## Pressure Piloted - vs - Bleed Piloted

Q: What is the difference between pressure piloted valves and bleed piloted valves?
A: Pressure piloting and bleed piloting refer to two different modes in which valves may be actuated. Pressure piloting positively actuates a directional valves by an external air signal that comes from a remote three-way valve, such as the Micro-Line valve series. Air pressure piloting provides an economical alternative to the use of electric switches and solenoids.


Bleed piloting uses internal air from the directional valve to feed the pilot valve. Air flows from the directional valve to the bleed valve. When the bleed valve is actuated, a pressure drop occurs in the directional valve pilot section. This causes a differential pressure and valve shift.


The main advantage of bleed piloting is that only one line enters the bleed valve. However, if the line is severed, a shift occurs. Pressure piloting is considered more positive and reliable.

## Low Force To Actuate

Q: Are there valves available that require an unusually low force to actuate?
A: Low-stress valves need only 6-8 oz. of force to initiate a signal. These valves reduce stress on worker's hands. LTV four-way valves operate on a pressure differential basis that allows them to actuate on very little force.

## Manual Overrides

Q: What are manual overrides in air valves used for?
A: Manual overrides permit the user to actuate the directional valves without using the switches or pilot valves that would normally be used. In this way, a circuit may be tested without actually moving the machine elements.


Both Capsula valves and Nova valves are available with manual overrides.

## Normally Closed - vs - Normally Open

Q: What is the difference between a three-way normally closed valve and a three-way normally open valve?
A: Normally open valves allow air to pass when not actuated. Normally closed valves allow air to pass only when they are actuated.


Normally Open Flow Pattern



Normally Closed Flow Pattern


## Panel Mounted



Q: Are there valves available that fit through "knockouts" in control panels?
A: MV 3-way valves and LTV 4-way valves have threaded mounting stems for panels.

## External Air Supply For Solenoids



Q: Under what conditions should an external air supply be used to feed the solenoids on a directional valve?
A: When the air pressure passing through the power section of the valve is insufficient to shift the spool, when the medium passing through the power section would be detrimental to the solenoid operator, or where the operating medium could not be exhausted to the atmosphere.

## Size Selection



Example: Estimated force needed is 900 lbs . Air pressure to be used is 80 PSI :
80 PSI x Power Factor = 900 lbs.
Power Factor $=900 \mathrm{lbs} / 80 \mathrm{PSI}=11.25$
The power factor just above 11.25 is 12.6 . Therefore, this job will require a $4^{\prime \prime}$ bore cylinder.

## Piston Rod Strength

If subjected to a heavy load a piston rod may buckle. The following chart suggests minimum rod diameter under various load conditions and when the rod is extended and unsupported and must be used in accordance with the chart's instructions. (see next paragraph). There must be no side load or bend stress at any point along the extending rod.

HOW TO USE THE TABLE: Exposed length of rod is shown at the top of the table. This length is typically longer than the stroke length of the cylinder. The vertical scale shows the load on the cylinder and is in English tons ( 1 ton $=2000 \mathrm{lbs}$.) If the rod and and front end of the cylinder barrel are rigidly supported, then a smaller rod will be sufficient; use the column that is $1 / 2$ the length of the actual piston rod. If pivot to pivot mounting is used, double the the actual length of the exposed rod and utilize the suggest rod diameter.

Figures in body of chart are suggested minimum rod diameters

|  | Exposed Length of Piston Rod (IN) |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tons | 10 | 20 | 40 | 60 | 70 | 80 | 100 | 120 |
| $1 / 2$ | $3 / 4$ |  |  |  |  |  |  | 1 |
| $3 / 4$ | $13 / 16$ |  |  |  |  |  |  | $1-1 / 16$ |
| 1 | 5 | $7 / 8$ | $1-1 / 8$ | $1-1 / 4$ | $1-3 / 8$ |  |  |  |
| $1-1 / 2$ |  | $11 / 16$ | $15 / 16$ | $1-3 / 16$ | $1-3 / 8$ | $1-1 / 2$ |  |  |
| 2 |  | $3 / 4$ | 1 | $1-1 / 4$ | $1-7 / 16$ | $1-9 / 16$ | $1-3 / 16$ |  |
| 3 | $13 / 16$ | $7 / 8$ | $1-1 / 8$ | $1-3 / 8$ | $1-9 / 16$ | $1-5 / 8$ | $1-7 / 8$ |  |
| 4 | $15 / 16$ | 1 | $1-3 / 16$ | $1-1 / 2$ | $1-5 / 8$ | $1-3 / 4$ | 2 | $2-1 / 4$ |
| 5 | 1 | $1-1 / 8$ | $1-5 / 16$ | $1-9 / 16$ | $1-3 / 4$ | $1-7 / 8$ | $2-1 / 8$ | $2-3 / 8$ |
| $7-1 / 2$ | $1-3 / 16$ | $1-1 / 4$ | $1-7 / 16$ | $1-3 / 4$ | $1-7 / 8$ | 2 | $2-1 / 4$ | $2-1 / 2$ |
| 10 | $1-3 / 8$ | $1-7 / 16$ | $1-5 / 8$ | $1-7 / 8$ | 2 | $2-1 / 8$ | $2-7 / 16$ | $2-3 / 4$ |
| 15 | $1-1 / 16$ | $1-3 / 4$ | $1-7 / 8$ | $2-1 / 8$ | $2-1 / 4$ | $2-3 / 8$ | $2-11 / 16$ | 3 |
| 20 | 2 | 2 | $2-1 / 8$ | $2-3 / 8$ | $2-1 / 2$ | $2-5 / 8$ | $2-7 / 8$ | $3-1 / 4$ |
| 30 | $2-3 / 8$ | $2-7 / 16$ | $2-1 / 2$ | $2-3 / 4$ | $2-3 / 4$ | $2-7 / 8$ | $3-1 / 4$ | $3-1 / 2$ |
| 40 | $2-3 / 4$ | $2-3 / 4$ | $2-7 / 8$ | 3 | 3 | $3-1 / 4$ | $3-1 / 2$ | $3-3 / 4$ |
| 50 | $3-1 / 8$ | $3-1 / 8$ | $3-1 / 4$ | $3-3 / 8$ | $3-1 / 2$ | $3-1 / 2$ | $3-3 / 4$ | 4 |
| 75 | $3-3 / 4$ | $3-3 / 4$ | $3-7 / 8$ | 4 | 4 | $4-1 / 8$ | $4-3 / 8$ | $4-1 / 2$ |
| 100 | $4-3 / 8$ | $4-3 / 8$ | $4-3 / 8$ | $4-1 / 2$ | $4-3 / 4$ | $4-3 / 4$ | $4-7 / 8$ | 5 |
| 150 | $5-3 / 8$ | $5-3 / 8$ | $5-3 / 8$ | $5-1 / 2$ | $5-1 / 2$ | $5-1 / 2$ | $5-3 / 4$ | 6 |

CAUTION: Horizontal or angle mounted cylinders (anything other than vertical) creates a bend stress on the rod when extended, just from the weight of the rod and cylinder itself. Trunnion mounting should be utilized in a position which will balance the cylinder weight when extended.

## Pneumatic Cylinder Force

Cylinder forces are shown in pounds for both extension and retraction. Lines standard type show extension forces, using the full piston area. Lines in italic type show retraction forces with various rod sizes. The valves below are theoretical, derived by calculation.

Pressures shown across the top of the chart are differential pressures across the two cylinder ports. In practice, the air supply line must supply another 5\% of pressure to make up for cylinder loss, and must supply an estimated $25-50 \%$ additional pressure to make up for flow losses in lines and valving so the cylinder will have sufficient travel speed.

For all practical purposes design your system $25 \%$ over and above your theoretical calculations.

| Piston Dia. | Rod <br> Dia | Effec. <br> Area <br> Sq. In. | $\begin{gathered} 60 \\ \text { PSI } \end{gathered}$ | $\begin{gathered} 70 \\ \text { PSI } \end{gathered}$ | $\begin{gathered} 80 \\ \text { PSI } \end{gathered}$ | $\begin{gathered} 90 \\ \text { PSI } \end{gathered}$ | $\begin{array}{r} 100 \\ \text { PSI } \end{array}$ | 110 PSI | $\begin{array}{r} 120 \\ \text { PSI } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-1/2 | None | 1.77 | 106 | 124 | 142 | 159 | 177 | 195 | 230 |
|  | 5/8 | 1.46 | 88 | 102 | 117 | 132 | 146 | 161 | 190 |
|  | 1 | 0.99 | 59 | 69 | 79 | 89 | 98 | 108 | 128 |
| 2 | None | 3.14 | 188 | 220 | 251 | 283 | 314 | 345 | 377 |
|  | 5/8 | 2.83 | 170 | 198 | 227 | 255 | 283 | 312 | 340 |
|  | 1 | 2.35 | 141 | 165 | 188 | 212 | 235 | 259 | 283 |
| 2-1/2 | None | 4.91 | 295 | 344 | 393 | 442 | 491 | 540 | 589 |
|  | 5/8 | 4.60 | 276 | 322 | 368 | 414 | 460 | 506 | 552 |
|  | 1 | 4.12 | 247 | 289 | 330 | 371 | 412 | 454 | 495 |
| 3 | None | 7.07 | 424 | 495 | 565 | 636 | 707 | 778 | 848 |
|  | 5/8 | 6.76 | 406 | 431 | 540 | 608 | 676 | 744 | 814 |
| 3-1/4 | None | 8.30 | 498 | 581 | 664 | 747 | 830 | 913 | 996 |
|  | 1 | 7.51 | 451 | 526 | 601 | 676 | 751 | 826 | 902 |
|  | 1-3/8 | 6.82 | 409 | 477 | 545 | 613 | 681 | 818 | 818 |
| 4 | None | 12.57 | 754 | 880 | 1006 | 1131 | 1257 | 1283 | 1508 |
|  | 1 | 11.78 | 707 | 825 | 943 | 1061 | 1178 | 1296 | 1415 |
|  | 1-3/8 | 11.09 | 665 | 776 | 887 | 998 | 1109 | 1219 | 1330 |
| 5 | None | 19.64 | 1178 | 1375 | 1571 | 1768 | 1964 | 2160 | 2357 |
|  | 1 | 18.85 | 1131 | 1320 | 1508 | 1697 | 1885 | 2074 | 2263 |
|  | 1-3/8 | 18.16 | 1089 | 1271 | 1452 | 1634 | 1816 | 1997 | 2179 |
| 6 | None | 28.27 | 1696 | 1979 | 2262 | 2544 | 2827 | 3110 | 3392 |
|  | 1-3/8 | 26.79 | 1607 | 1875 | 2143 | 2411 | 2679 | 2946 | 3214 |
|  | 1-3/4 | 25.90 | 1552 | 1811 | 2069 | 2328 | 2586 | 2845 | 3104 |
| 8 | None | 50.27 | 3016 | 3519 | 4022 | 4524 | 5027 | 5530 | 6032 |
|  | 1-3/8 | 48.79 | 2927 | 3415 | 3903 | 4391 | 4879 | 5366 | 5854 |
|  | 1-3/4 | 47.90 | 2872 | 3351 | 3829 | 4308 | 4786 | 5265 | 5744 |
| 10 | None | 78.54 | 4712 | 5498 | 6283 | 7069 | 7854 | 8639 | 9425 |
|  | 1-3/4 | 76.14 | 4568 | 5329 | 6091 | 6852 | 7614 | 8375 | 9136 |
|  | 2 | 75.40 | 4524 | 5278 | 6032 | 6786 | 7540 | 8294 | 9048 |
| 12 | None | 113.10 | 6786 | 7917 | 9048 | 10179 | 11310 | 12441 | 13572 |
|  | 2 | 110.00 | 6598 | 7697 | 8797 | 9896 | 10996 | 12095 | 13195 |
|  | 2-1/2 | 108.20 | 6491 | 7573 | 8655 | 9737 | 10819 | 11901 | 12983 |

## Air Cylinder Speed

Estimating cylinder speed is extremely difficult because of the flow losses within the system in piping, fittings, and porting through the valves which are in the air path. Flow losses cause a loss in pressure which directly effect the force output. To be able to determine the maximum speed of the cylinder, the sum of all flow losses, pressure required for the force output and the available inlet pressure must be known. Circuit losses cannot be determined or calculated accurately. Rules of Thumb are relied upon to determine an approximation of air cylinder speed.

The first general rule of thumb is chose a cylinder which will allow for at least $25 \%$ more force then what is required. For extremely fast operations, chose a cylinder which will allow for $50 \%$ more force than what is required. This will leave $25 \%$ or $50 \%$ of inlet pressure to satisfy system losses.

The second rule of thumb is to select a directional control valve which has the same port size as the cylinder which it will be operating. Typically larger valves internal flow capacity is the same as the connection size. On smaller valves ,the internal flow capacity is typically much less than the connection size. Always be sure to check the valves flow rate, and do not relay on the port size.

## ESTIMATED CYLINDER SPEED

Figures below are in Inches per Second

| Actual Valve Orifice Dia. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bore | $1 / 32$ | $1 / 16$ | $1 / 8$ | $1 / 4$ | $3 / 8$ | $1 / 2$ | $3 / 4$ | 1 |
| 1 | 6 | 15 | 37 |  |  |  |  |  |
| $1-1 / 8$ | 5 | 12 | 28 | 85 |  |  |  |  |
| $1-1 / 2$ | 3 | 7 | 16 | 50 |  |  |  |  |
| 2 |  | 4 | 9 | 28 | 70 |  |  |  |
| $2-1 / 2$ |  |  | 6 | 18 | 45 | 72 |  |  |
| 3 |  |  | 4 | 12 | 30 | 48 |  |  |
| $3-1 / 4$ |  |  | 3 | 10 | 24 | 37 | 79 |  |
| 4 |  |  |  | 7 | 17 | 28 | 60 |  |
| 5 |  |  |  | 4 | 11 | 18 | 40 | 82 |
| 6 |  |  |  | 3 | 7 | 12 | 26 | 55 |
| 8 |  |  |  |  | 4 | 7 | 15 | 32 |
| 10 |  |  |  |  |  | 4 | 9 | 20 |
| 12 |  |  |  |  |  | 3 | 6 | 14 |

NOTE: These values are an approximate speed, under average conditions, where the force required is $50 \%$ of available 80-100 PSI inlet pressure, the directional valve internal flow is equal to the porting and an unlimited supply of air. Acceleration distance is assumed to be relatively short compared to total stroke based upon sufficiently long stroke.

## Estimate Travel Speed of Loaded Air Cylinder

## Air Flow Through Orifices

The chart below gives theoretical SCFM air flow through sharp edged orifices. In actual practice, approximately $2 / 3$ of this flow is obtained. Assume $75 \%$ of line pressure (PSI) is actually working on the load. The remaining $25 \%$ is consumed by flow losses in the valve, and connecting lines.

Calculate $75 \%$ of your line pressure (PSI) and find it in the first column in the chart below. Move across the table to the column which is the actual port size of your valve. Since valves do not contain sharp edged orifices, divide this number in half.

After finding the SCFM, convert this to CFM at the pressure required to move the load. From this the speed of travel can be estimated.

## Approximate SCFM flow though Sharp Edged Orifices

| PSI <br> Across | Orifice Diameter, in Inches |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Orifice | 1/64 | 1/32 | 1/16 | 1/8 | 1/4 | 3/8 | 1/2 | 5/8 | 3/4 | 7/8 | 1 |
| 5 | 0.062 | 0.249 | 0.993 | 3.97 | 15.9 | 35.7 | 63.5 | 99.3 | 143 | 195 | 254 |
| 6 | 0.068 | 0.272 | 1.09 | 4.34 | 17.4 | 39.1 | 69.5 | 109 | 156 | 213 | 278 |
| 7 | 0.073 | 0.293 | 1.17 | 4.68 | 18.7 | 42.2 | 75.0 | 117 | 168 | 230 | 300 |
| 9 | 0.083 | 0.331 | 1.32 | 5.30 | 21.2 | 47.7 | 84.7 | 132 | 191 | 260 | 339 |
| 12 | 0.095 | 0.379 | 1.52 | 6.07 | 24.3 | 54.6 | 97.0 | 152 | 218 | 297 | 388 |
| 15 | 0.105 | 0.420 | 1.68 | 6.72 | 26.9 | 60.5 | 108 | 168 | 242 | 329 | 430 |
| 20 | 0.123 | 0.491 | 1.96 | 7.86 | 31.4 | 70.7 | 126 | 196 | 283 | 385 | 503 |
| 25 | 0.140 | 0.562 | 2.25 | 8.98 | 35.9 | 80.9 | 144 | 225 | 323 | 440 | 575 |
| 30 | 0.158 | 0.633 | 2.53 | 10.1 | 40.5 | 91.1 | 162 | 253 | 365 | 496 | 648 |
| 35 | 0.176 | 0.703 | 2.81 | 11.3 | 45.0 | 101 | 180 | 281 | 405 | 551 | 720 |
| 40 | 0.194 | 0.774 | 3.10 | 12.4 | 49.6 | 112 | 198 | 310 | 446 | 607 | 793 |
| 45 | 0.211 | 0.845 | 3.38 | 13.5 | 54.1 | 122 | 216 | 338 | 487 | 662 | 865 |
| 50 | 0.229 | 0.916 | 3.66 | 14.7 | 58.6 | 132 | 235 | 366 | 528 | 718 | 938 |
| 60 | 0.264 | 1.06 | 4.23 | 16.9 | 67.6 | 152 | 271 | 423 | 609 | 828 | 1082 |
| 70 | 0.300 | 1.20 | 4.79 | 19.2 | 76.7 | 173 | 307 | 479 | 690 | 939 | 1227 |
| 80 | 0.335 | 1.34 | 5.36 | 21.4 | 85.7 | 193 | 343 | 536 | 771 | 1050 | 1371 |
| 90 | 0.370 | 1.48 | 5.92 | 23.7 | 94.8 | 213 | 379 | 592 | 853 | 1161 | 1516 |
| 100 | 0.406 | 1.62 | 6.49 | 26.0 | 104 | 234 | 415 | 649 | 934 | 1272 | 1661 |
| 110 | 0.441 | 1.76 | 7.05 | 28.2 | 113 | 254 | 452 | 705 | 1016 | 1383 | 1806 |
| 120 | 0.476 | 1.91 | 7.62 | 30.5 | 122 | 274 | 488 | 762 | 1097 | 1494 | 1951 |
| 130 | 0.494 | 1.98 | 7.90 | 31.6 | 126 | 284 | 506 | 790 | 1138 | 1549 | 2023 |

## Air Consumption Rates

Q: How do I calculate the air consumption of a cylinder?
Example: Determine the air consumption of a $2^{\prime \prime}$ bore cylinder with a $4^{\prime \prime}$ stroke operating 30 complete cycles (out and back) per minute at 80 PSI inlet pressure.
A:

1. Find the area of the piston by converting the bore diameter into square inches. $(2 \mathrm{in} \text {. bore/2 })^{2} \times 3.1416(\Pi)=3.14 \mathrm{sq}$. in.
2. Determine consumption per single stroke.
3.14 sq. in. $\times 4$ in. stroke $=12.56$ cu.in.
3. Determine consumption per complete cycle (Disregard displacement of piston rod because it is generally not significant).
12.56 cu.in. $\times 2=25.12$ cu.in. per cycle
4. Determine volume of 80 PSI air that is consumed per minute.
25.12 cu.in. $\times 30$ cycles $/$ minute $=753.6$ cu.in. $/ \mathrm{min}$. of 80 PSI air
5. Convert cu.in. to cu.ft.
753.6 cu.in. $/ \mathrm{min} .=0.436 \mathrm{cu} . \mathrm{ft} . / \mathrm{min}$.

1728 cu.in/cu.ft.
6. Convert air compressed to 80 PSI to "free" (uncompressed) air. 80 PSI +14.7 PSI $=6.44$ (times air is compressed when at 80 PSI)

### 14.7 PSI

7. Determine cubic feet of free air used per minute.
0.436 cu . ft. $\times 6.44$ compression ratio $=2.81 \mathrm{cu}$. ft. of free air used per minute
8. So, the consumption rate of a $2^{\prime \prime}$ bore, $4^{\prime \prime}$ stroke cylinder operating 30 complete cycles per minute at 80 PSI is $\mathbf{2 . 8 1}$ SCFM (Standard Cubic Feet Per Minute) of free air. "Standard" means at a temperature of $70^{\circ} \mathrm{F}$ and at sea level. Also see questions regarding $\mathrm{C}_{\mathrm{v}}$ (pg. 1) and cylinder size selection (pg. 10).

## Determine Air Volume Required

The figures in the table below are for cylinders with standard rods. The difference with over-sized rods is negligible. Air consumption was calculated assuming the cylinder would dwell momentarily at the end of each stroke, allowing air to fill up the cylinder to set system pressure. If cylinder strokes prior to allowing for air to fill, air consumption will be less. than what is shown in the table.

Assuming system losses through piping and valves will be approximately $25 \%$, make sure that the cylinder bore selected will balance the load at $75 \%$ of the pressure available in the system. Without this surplus pressure the cylinder may not travel at it desired speed.

## Using the Table Below

Upon determining the regulator pressure, go to the proper column. The figures below represent a $1^{\prime \prime}$ stroke, extend and retract cycle. Take the figure and multiply times the actual stroke and by the number of cycles needed in one minute. The result will be the SCFM for the application.

Cylinder Air Consumption: 1 " Stroke, Full Cycle

| Cylinder | $\mathbf{6 0}$ | $\mathbf{7 0}$ | $\mathbf{8 0}$ | $\mathbf{9 0}$ | $\mathbf{1 0 0}$ | $\mathbf{1 1 0}$ | $\mathbf{1 2 0}$ | $\mathbf{1 3 0}$ | $\mathbf{1 4 0}$ | $\mathbf{1 5 0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bore | PSI | PSI | PSI | PSI | PSI | PSI | PSI | PSI | PSI | PSI |
| 1.50 | 0.009 | 0.010 | 0.012 | 0.013 | 0.015 | 0.016 | 0.017 | 0.018 | 0.020 | 0.021 |
| 2.00 | 0.018 | 0.020 | 0.022 | 0.025 | 0.027 | 0.029 | 0.032 | 0.034 | 0.036 | 0.039 |
| 2.50 | 0.028 | 0.032 | 0.035 | 0.039 | 0.043 | 0.047 | 0.050 | 0.054 | 0.058 | 0.062 |
| 3.00 | 0.039 | 0.044 | 0.050 | 0.055 | 0.060 | 0.066 | 0.070 | 0.076 | 0.081 | 0.087 |
| 3.25 | 0.046 | 0.053 | 0.059 | 0.065 | 0.071 | 0.078 | 0.084 | 0.090 | 0.096 | 0.102 |
| 4.00 | 0.072 | 0.081 | 0.091 | 0.100 | 0.110 | 0.119 | 0.129 | 0.139 | 0.148 | 0.158 |
| 5.00 | 0.113 | 0.128 | 0.143 | 0.159 | 0.174 | 0.189 | 0.204 | 0.219 | 0.234 | 0.249 |
| 6.00 | 0.162 | 0.184 | 0.205 | 0.227 | 0.249 | 0.270 | 0.292 | 0.314 | 0.335 | 0.357 |
| 8.00 | 0.291 | 0.330 | 0.369 | 0.408 | 0.447 | 0.486 | 0.525 | 0.564 | 0.602 | 0.642 |
| 10.00 | 0.455 | 0.516 | 0.576 | 0.637 | 0.698 | 0.759 | 0.820 | 0.881 | 0.940 | 1.000 |
| 12.00 | 0.656 | 0.744 | 0.831 | 0.919 | 1.010 | 1.090 | 1.180 | 1.270 | 1.360 | 1.450 |

Example: What is the SCFM of a cylinder in a stamping application, that moves a 2250 lbs . wieght 60 times per minute through a $6^{\prime \prime}$ stoke?

By selecting a $6^{\prime \prime}$ bore, the 2250 lbs . force is realized at 80 PSI . Then add $25 \%$ more pressure ( 20 PSI), to account for system losses and set the regulator at 100 PSI. Then using the table above we have the following calculation:
$0.249 \times 6$ (stroke) $\times 60$ (cycles per minute) $=89.64$ SCFM

## Double-Acting -vs- Single-Acting



Q: What are the differences between double-acting and singleacting cylinders?
A: Double-acting cylinders provide power on both the "extend" and "retract" stroke. They require the use of four way directional control valves.

Single-acting cylinders provide power only on the "push" stroke. The piston rod is returned by an internal spring. Single-acting cylinders use about one-half as much air as double-acting cylinders and are operated by 3-way valves.
NOTE: Valves Shown here are from the Nova Series (Four-Way Valve) and the MV Series (Three-Way Valve).

## Force Output Calculation

Q: How do I figure out the theoretical force output of a cylinder?
A: Follow these steps.

1. Calculate the area of the cylinder piston

$$
\begin{aligned}
& \text { Area }=\Pi r^{2} \\
& \text { where } \Pi=3.1416 \\
& r=1 / 2 \text { the bore diameter }
\end{aligned}
$$

2. Multiply the piston area by the air pressure to be used.

$$
\text { Area } \times \text { Pressure }=\text { Force Output }
$$

Example: What is the theoretical force output of a $2^{1} / 2^{\prime \prime}$ bore cylinder operating at 80 lbs . per square inch air pressure?

| Step 1. $\quad$ Area | $=\Pi r^{2}$ Area $=3.1416 \times 1.25^{2}$ |
| ---: | :--- |
| Area | $=4.91$ square inches |

Step 2. 4.91 sq. in. $\times 80 \mathrm{PSI}=393 \mathrm{lbs}$. of force
Note: The force output on the rod end of a cylinder will be slightly less due to the displacement of the rod.The real force output of a cylinder will be less than the theoretical output because of internal friction and external side loading.lt is best to use a cylinder that will generate from $25 \%$ to $50 \%$ more force than theoretically needed.

## Mid-Stroke Position Sensing

Q: How do I sense the position of a cylinder piston when it is somewhere between its limits?
A: Order your cylinder with Hall Effect or Reed switches and a magnetic piston. Set the switches at the desired trip points. An electrical signal will be emitted when the magnetic piston passes a switch.

## Non Lubricated



Q: Are there cylinders available that do not require lubrication?
A: Centaur cylinders have Teflon ${ }^{\circledR}$ seals that glide over the cylinder tube surface without the aid of a lubricant. Other cylinders have a "non-lube" option.

## Smoother Cylinder Motion



Q: What could cause a cylinder to move erratically during stroking?
A: Irregular rod motion could be caused by:

1. Too low an input air pressure for the load being moved.
2. Too small a cylinder bore size for the load being moved.
3. Side loading on the cylinder rod caused by misalignment of the rod and load.
4. Using flow control valves to meter the incoming air rather than the exhausting air.
5. Flow control valves are set for too slow a rod movement.
6. An absence of lubrication.

## Speed Boost

Q: How do I get more speed out of a cylinder?
A: You may increase the inlet pressure to within the recommended limits and/or you may place a quick exhaust valve in either or both cylinder port(s).


## Speed Control

 SILENCERS

Q: How can I control cylinder speed?
A: Use any of the following methods:

1. Place Dyla-Trol ${ }^{\circledR}$ flow control valves in each cylinder port. Install them so that the air leaving the cylinder is controlled.
2. Use right-angle flow controls in the cylinder ports. These feature recessed screw driver adjustment and convenient swivel for ease of tubing alignment.
3. Place speed control silencers into the exhaust ports of the control valve that is being used to power the cylinder.
4. Purchase a directional valve that has built-in-flow controls. See Dura-Matic Valves.

See Page 7, Flow Controls.

## Cushioning



Q: How do I prevent a cylinder from impacting at the end of its stroke?
A: Generally, it is best to order your cylinders with built-in cushions if you anticipate unacceptable end-of-stroke impact. Cushions decelerate the piston rod through the last ${ }^{11} / 66^{\prime \prime}$ of stroke. The degree of cushioning may be adjusted by means of a needle control in the cylinder head.

DM1, DM2 and HD1 Series cylinders offer adjustable cushion cylinders. Centaur cylinders are all supplied with rubber bumpers at no extra charge. Adjustable cushions and bumpers eliminate the "clank" that occurs at stroke completion.

## Position Sensing, End-Of-Stroke

Q: How do I sense that a cylinder rod has reached the end of its stroke?
A: Use any of the following methods or external limit valves:


1. Order your cylinder with Inter-Pilots ${ }^{\circledR}$. A built-in, normally closed, 3way valve that emits an air signal when the stroke limit is reached. Inter-Pilots ${ }^{\circledR}$ are available on the DM1, DM2 and HD1 cylinders. Note: To use Inter-Pilots ${ }^{\circledR}$, the full stroke of the cylinder must be used. 2. Order your cylinder with Hall Effect or Reed switches that emit electrical signals when the stroke limit is reached. Note: To use Hall Effect or Reed switches, the cylinder must be supplied with a magnetic piston.
2. Use stroke completion sensors. These valves react to pressure drops so that an output signal will be generated even if the piston is stopped short of a complete stroke.

## Increasing Power

Q: How do I get more power out of a particular cylinder?
A: You should increase the pressure of the air that feeds the cylinder within the recommended limits.


NOTE: The Control Valve shown here is from the Nova Series.

## Pressure Maintenance

Q: How do I maintain a constant cylinder force output when my air pressure supply fluctuates?
A: Set an air regulator ahead of your valve at a pressure that may always be maintained.


Example: Depending on the time of day and workload, a plant's air pressure fluctuates between 80 and 95 PSI. Set the regulator at 80 PSI and the cylinder power output through the plant will remain constant. Also, an air reservoir may be used to solve an air shortage problem. By mounting a reservoir close to a cylinder, an adequate amount of air will be supplied when needed.

## Reciprocating

Q: How do I get a cylinder to reciprocate automatically?
A: Order your cylinder with Inter-Pilots ${ }^{\circledR}$, Hall Effect or Reed switches, or stroke completion sensors. These devices will send signals to double pressure or solenoid operated valves that will shift each time a stroke has been completed. Reciprocation may also be achieved by having a cam, mounted on the cylinder rod, trip external limit valves.


NOTE: The Valve shown here is from the Nova Series. The 3-Way Limit Valves are from the MV series.


## Adjustable Stroke

Q: Is it possible to make the stroke of a cylinder adjustable?
A: Yes. Double-acting cylinders may be ordered with a common rod that protrudes from both cylinder end caps. A nut may be placed on one rod end to retain spacers that will limit the stroke distance. Be sure to guard the spacer end because "pinch points" will be present. DM1, DM2 and HD1 Cylinders are double acting.

## Single and Double Rods



Q: What is the difference between a single and double-rod cylinder?
A: Single-rod cylinders have a piston rod protruding from only one end of the cylinder. Double-rod cylinders have a common rod, driven by a single piston, protruding from both cylinder end caps. When one end retracts, the other extends. They are excellent for providing an adjustable stroke and providing additional rigidity. Also, a double-rod with attached cam may be used to trip a limit switch.

Space Conserving Type


SPACE SAVER ${ }^{\circledR}$


STANDARD CYL.

Q: I have a space problem and cannot fit a regular cylinder into the area available. What can I do?
A: Use the ultra-compact "Space-Saver" cylinder.

## Side Load Reduction



Q: How may I minimize the adverse effects of cylinder side loading?
A: First, be sure that the object being moved is in exact alignment with the piston rod. if the cylinder is rigidly mounted and the rod is forced off line, the cylinder bearing will wear prematurely and a loss of power will occur. It may be helpful to use guide rails to keep the object being moved in proper alignment.
Second, don't use all of the stroke. Particularly on pivot and clevis models, it is wise to have the piston stop a few inches short of full stroke. This makes the cylinder more rigid and extends bearing life.
Third, order your cylinder with an external bearing.
An external bearing takes advantage of physics by providing more bearing surface and a longer lever point than a standard cylinder type. (Order HD1 (Heavy Duty Air Cylinders)) Fourth, Order a Self Aligning Rod Coupler.

The Table on the right shows the Rod Couplers that offers. The thread shown is a male / female thread as the coupler has both a male and female end.

| Rod Couplers |  |
| :--- | :---: |
| Part \# | Rod Thread |
| DMA-312 | $5 / 6-24$ |
| DMA-375 | $3 / 8-24$ |
| DMA-437 | $7 / 6-20$ |
| DMA-500 | $1 / 2-20$ |
| DMA-625 | $5 / 8-18$ |
| DMA-750 | $3 / 4-16$ |
| DMA-875 | $7 / 8-14$ |
| DMA-1000 | $1-14$ |
| DMA-1250 | $11 / 4-12$ |

## High Temperature Operations

Q: I have an application in a high temperature environment. What should I do to avoid complication?
A: The control valve powering the cylinder should be mounted as far away from the heat as possible. While temperatures exceeding $100^{\circ} \mathrm{C}\left(212^{\circ} \mathrm{F}\right)$ can cause breakdown in Buna N seals, most cylinders may be supplied with fluorocarbon seals instead of Buna N. Fluorocarbon seals are effective to $204^{\circ} \mathrm{C}\left(400^{\circ} \mathrm{F}\right)$. Flurocarbon seals are also known as Viton ${ }^{\circledR}$ seals.

## Non-Lubricated Air Circuit



Q: Is it possible to build an air circuit using components that do not require lubrication?
A: Micro-Line pilot valves (MV), Capsula directional valves, and Centaur cylinders will provide excellent service without lubrication. Most cylinders are available with optional non-lube seals.

## Cylinder Presses, Non-Rotating

Q: How do I prevent the tooling attached to my air press rod from turning?
A: Order the press cylinder with a non-rotating rod option.


## Collet Fixtures



Q: Is there a way of firmly holding smooth round bars with an air powered device?
A: Use an air collet fixture. The device operates just like a double acting cylinder; air to close and open. The collet fixture uses standard industrial collets and can not only handle round bars but also hex bars.

## Basic Control Circuits

## Air Circuitry

Q: What is a typical air circuit?
A: The simplest and most common air circuit consists of a double-acting cylinder which is controlled by a four-way directional valve. The directional valve is actuated by air pilot valves or electric switches.


## Timing Circuits



In this circuit, the 3-way valve is actuated and air is sent to the control valve. The control valve shifts, sending air to the rear of the cylinder causing the cylinder to extend. Air also flows to the timer where it begins to time to the pre-setting. Once reached, the timer opens, allowing the air to flow through to the control valves other pilot port, shifting the valve back. Air flows through port B, retracting the cylinder.


Sample Components
Normally Open Timer - KLH-105
Control Valve - N2-SP

In this circuit a constant air signal is sent to the timer. The normally open timer allows air to flow through until the set time period expires. While air flows to the pilot of the control valve the cylinder extends and remains extended. When the time period expires the cylinder returns even if the air signal remains. NOTE: In this set-up if the air signal is removed before the timer, the cylinder will retract. The circuit will only recycle once the air signal is removed and re-applied.

## Dual Signal Circuit



Sample Components 3-Way Pilot Valve - MV-140 Control Valve - N2-DP Impulse Relay - 414B 3-Way Limit Valve - MV-15

When actuated, the 3 -way valve sends a signal to 414B, which emits a signal to the control valve. The 3-way valve remains actuated. The valve shifts, allowing air to flow through port A, extending the cylinder. 414B senses the back pressure caused by the shifted valve, closes, and exhausts. Since the signal from valve \#1 is blocked by the closed 414B, valve \#2 (when actuated) shifts the control valve back. Air flows through port B, retracting the cylinder.

## 2 Valves for 3 Position Function

Use these set-ups to obtain a Three Position Function with (2) Two Position valves. The circuitry shown is ideal for use with the Isonic product line.

## Pressure Applied Set-Up

Actuate Valve \#1 for Retraction; Actuate Vavle \#2 for Extension.
Supply pressure must be equal on both valve \#1 and \#2.


## Pressure Relieved Set-Up

Actuate Valve \#1 for Extension; Actuate Valve \#2 for Retraction.
Supply pressure does not have to be equal.


For an All Ports Blocked Three Position Function, an additional 2-way valve must be used as for blocking the exhaust of the two valves. This 3rd valve is actuated when ever either one of the other valves is actuated.

## Two Hand Extend One Hand Retract

For applications where a secondary operation must occur, utilize this circuit. This circuit allows for the operator to be "tied down" during the clamping of a part via the actuation of the two hand control. Once the rod movement has stopped, the operator can the move onto the secondary operation.

Additionally with the use of the stroke completion sensor the circuit will work even if clamping on material that is not consistently the same size.


The Bill Of Materials to the left can be used to mix and match for your specific application. Additionally multiple components maybe added at "D". (Example: Timer and Push Button combination for an automatic return or manual return.)

| A | CSV-101 <br> CSV-101 LS <br> CSV 107 LS1 <br> CSV 107 LS2 | 2 Hand Anti- Tie Down Control Unit <br> Same as above, but with low stress buttons <br> Same as CSV-101, but w/ remote buttons <br> Same above but/ with low force actuators |
| :--- | :--- | :--- |
| B | SV-1 | Shuttle valve |
| C | N2-SP <br> C2-3 <br> C5-3 | $1 / 4^{\prime \prime}$ port spring return <br> $1 / 4^{\prime \prime}$ port spring return, rugged applications <br> $1 / 2^{\prime \prime}$ port spring return, rugged applications |
| D | MV-140 <br> MV-ES <br> KLH-105 <br> MV- | Emergency Stop <br> Timer 1-10 sec. <br> Any MV- type Valve will work here, set up Normally Open |
| E | SCS-112 <br> SCS-250 <br> SCS-375 <br> SCS-500 | $1 / 8^{\prime \prime}$ Stroke Completion Sensor (SCS) <br> $3 / 8^{\prime \prime}$ SCS <br> $1 / 22^{\prime \prime}$ SCS |

Use this circuit, where a "pinch point" exists on both the extension and retraction of the linear actuator. This circuit will require the operator to use the two hand control for either motion.

The suggested components will accommodate up to one 4" bore cylinder with relatively good speed.

Operation:

1) Operator sets " $B$ " valve to either extend or retract cylinder.
2) Operator uses " $A$ " (two hand control) to move cylinder.
3) If one or both buttons are not actuated cylinder will stop in place.


| A | CSV-101 <br> CSV-101 LS <br> CSV 107 LS1 <br> CSV 107 LS2 | 2 Hand Anti- Tie Down Control Unit <br> Same as above, but with low stress buttons <br> Same as CSV-101, but w/ remote buttons <br> Same as above but/ with low force actuators |
| :--- | :--- | :--- |
| B | MV-35 <br> MV-TP | Two Position Detented 3-Way Valve <br> Two Position Detented 3-Way Valve |
| C | C2-2H | Three Position Spring Centered 4-Way Valve |

## 2 Hand Extend with Automatic Return

This Circuit is useful for applications where cycle time and safety is an issue. With the Automatic Return feature, the operators hands are tied down and the cylinder will return when the work is completed, not when the operator removes their hands from the actuator.

Operator uses CSV-102 (Two Hand Control) to the extend cylinder, if one or both hands are removed, cylinder returns. If limit is reached the cylinder will auto return even if the operators hand remain on the two hand control.


CSV-102 when actuated, pilots the Double Air Pilot 4-Way Valve to allow air to the Air Pilot Spring Return Valve. When released the CSV-102, pilots the Double Air Pilot 4-Way Valve back to the original position. The Impulse Relay takes the constant input from the CSV-102 and changes it to an impulse allowing for the auto-return from the Limit Switch.

Bill Of Material With Typical Components

| Component | Part Number |
| :--- | :---: |
| CSV-102 | CSV-102 |
| Impulse Relay | 414B |
| Double Air Pilot <br> 4-Way Valve | N2-DP |
| Shuttle Valve | SV-1 |
| Air Pilot, Spring <br> Return Valve | N2-SP |
| Limit Switch | MV Type |

The suggested components will accommodate up to a 4" Bore Cylinder.

## Pneumatic Pipe Size

The pipe sizes listed in the chart below are assuming a 100 PSI pneumatic system to carry air at a 1 PSI loss per 100 feet. Conservatively figure each pipe fitting to equal 5 feet of pipe. At pressures other than 100 PSI , flow capacity will be inversely proportionate to pressure (Calculated by Boyle's Law and based upon absolute PSIA Pressure levels).

| SCFM | Length of Run Feet |  |  |  |  |  |  |  | Compressor |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Flow | 25 | 50 | 75 | 100 | 150 | 200 | 300 | 500 | 100 | HP |
| 6 | $1 / 2$ | $1 / 2$ | $1 / 2$ | $1 / 2$ | $1 / 2$ | $1 / 2$ | $1 / 2$ | $3 / 4$ | $3 / 4$ | 1 |
| 18 | $1 / 2$ | $1 / 2$ | $1 / 2$ | $3 / 4$ | $3 / 4$ | $3 / 4$ | $3 / 4$ | 1 | 1 | 3 |
| 30 | $3 / 4$ | $3 / 4$ | $3 / 4$ | $3 / 4$ | 1 | 1 | 1 | $1-1 / 4$ | $1-1 / 4$ | 5 |
| 45 | $3 / 4$ | $3 / 4$ | 1 | 1 | 1 | 1 | $1-1 / 4$ | $1-1 / 4$ | $1-1 / 4$ | $7-1 / 2$ |
| 60 | $3 / 4$ | 1 | 1 | 1 | $1-1 / 4$ | $1-1 / 4$ | $1-1 / 4$ | $1-1 / 2$ | $1-1 / 2$ | 10 |
| 90 | 1 | 1 | $1-1 / 4$ | $1-1 / 4$ | $1-1 / 4$ | $1-1 / 4$ | $1-1 / 2$ | $1-1 / 2$ | 2 | 15 |
| 120 | 1 | $1-1 / 4$ | $1-1 / 4$ | $1-1 / 4$ | $1-1 / 2$ | $1-1 / 2$ | $1-1 / 2$ | 2 | 2 | 20 |
| 150 | $1-1 / 4$ | $1-1 / 4$ | $1-1 / 4$ | $1-1 / 2$ | $1-1 / 2$ | 2 | 2 | 2 | $2-1 / 2$ | 25 |
| 180 | $1-1 / 4$ | $1-1 / 2$ | $1-1 / 2$ | $1-1 / 2$ | 2 | 2 | 2 | $2-1 / 2$ | $2-1 / 2$ | 30 |
| 240 | $1-1 / 4$ | $1-1 / 2$ | $1-1 / 2$ | 2 | 2 | 2 | $2-1 / 2$ | $2-1 / 2$ | 3 | 40 |
| 300 | $1-1 / 2$ | 2 | 2 | 2 | 2 | $2-1 / 2$ | $2-1 / 2$ | 3 | 3 | 50 |
| 360 | $1-1 / 2$ | 2 | 2 | 2 | $2-1 / 2$ | $2-1 / 2$ | $2-1 / 2$ | 3 | 3 | 60 |
| 450 | 2 | 2 | 2 | $2-1 / 2$ | $2-1 / 2$ | 3 | 3 | 3 | $3-1 / 2$ | 75 |
| 600 | 2 | $2-1 / 2$ | $2-1 / 2$ | $2-1 / 2$ | 3 | 3 | 3 | $3-1 / 2$ | 4 | 100 |
| 750 | 2 | $2-1 / 2$ | $2-1 / 2$ | 3 | 3 | 3 | $3-1 / 2$ | $3-1 / 2$ | 4 | 125 |

Pneumatic Pressure Loss
Figures in the table below are approximate PSI compressed air pressure losses for every 100 feet of clean commercial steel pipe. (Schedule 40)

| CFM | $1 / 2 \mathrm{INCH}$ |  | $3 / 4$ | INCH | 1 INCH |  | $1-1 / 4$ |  | INCH | $1-1 / 2$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INCH |  |  |  |  |  |  |  |  |  |  |
| Free | 80 | 125 | 80 | 125 | 80 | 125 | 80 | 125 | 80 | 125 |
| Air | PSI | PSI | PSI | PSI | PSI | PSI | PSI | PSI | PSI | PSI |
| 10 | 0.45 | 0.30 | 0.11 | 0.08 | 0.04 | 0.02 |  |  |  |  |
| 20 | 1.75 | 1.15 | 0.40 | 0.28 | 0.15 | 0.08 |  |  |  |  |
| 30 | 3.85 | 2.55 | 0.90 | 0.60 | 0.30 | 0.20 |  |  |  |  |
| 40 | 6.95 | 4.55 | 1.55 | 1.05 | 0.45 | 0.30 |  |  |  |  |
| 50 | 10.50 | 7.00 | 2.40 | 1.60 | 0.75 | 0.50 | 0.18 | 0.12 |  |  |
| 60 |  |  | 3.45 | 2.35 | 1.00 | 0.70 | 0.25 | 0.17 |  |  |
| 70 |  |  | 4.75 | 3.15 | 1.35 | 0.90 | 0.35 | 0.23 | 0.16 | 0.10 |
| 80 |  |  | 6.15 | 4.10 | 1.75 | 1.20 | 0.45 | 0.30 | 0.20 | 0.14 |
| 90 |  |  | 7.75 | 5.15 | 2.25 | 1.50 | 0.56 | 0.40 | 0.25 | 0.17 |
| 100 |  |  | 9.60 | 6.35 | 2.70 | 1.80 | 0.65 | 0.45 | 0.30 | 0.20 |
| 125 |  |  | 15.50 | 9.80 | 4.20 | 2.80 | 1.05 | 0.70 | 0.45 | 0.32 |
| 150 |  |  | 23.00 | 14.50 | 5.75 | 4.00 | 1.45 | 1.00 | 0.65 | 0.45 |
| 175 |  |  |  |  | 8.10 | 5.45 | 2.00 | 1.30 | 0.90 | 0.60 |
| 200 |  |  |  |  | 10.90 | 7.10 | 2.60 | 1.75 | 1.15 | 0.80 |
| 250 |  |  |  |  |  |  | 4.05 | 2.65 | 1.80 | 1.20 |
| 300 |  |  |  |  |  |  |  | 7.90 | 5.15 | 3.55 |
| 350 |  |  |  |  |  |  | 10.30 | 6.75 | 4.55 | 3.05 |
| 400 |  |  |  |  |  |  |  |  | 5.80 | 3.80 |
| 450 |  |  |  |  |  |  |  |  |  |  |
| 500 |  |  |  |  |  |  |  |  |  |  |

## Air Flow Loss Through Pipes

Instructions: Find the factor from the chart below according to the pipe size and SCFM. Divide the factor by the Compression Ratio. Then multiply the number by the actual length of pipe, in feet, then divide by 1000. This result is the pressure loss in PSI.

Compression Ratio $=($ Gauge Pressure +14.5$) / 14.5$
Pressure Loss (PSI) $=$ Factor $/$ Compression Ratio $\times$ Length of Pipe $(F t) / 1000$
Factor Table

|  | Sipe Size NPT |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1 / 2$ | $3 / 4$ | 1 | $1-1 / 4$ | $1-1 / 2$ | $1-3 / 4$ | 2 | $2-1 / 2$ |
| 5 | 12.7 | 1.2 | 0.5 |  |  |  |  |  |
| 10 | 50.7 | 7.8 | 2.2 | 0.5 |  |  |  |  |
| 15 | 114 | 17.6 | 4.9 | 1.1 |  |  |  |  |
| 20 | 202 | 30.4 | 8.7 | 2.0 |  |  |  |  |
| 25 | 316 | 50.0 | 13.6 | 3.2 | 1.4 | 0.7 |  |  |
| 30 | 456 | 70.4 | 19.6 | 4.5 | 2.0 | 1.1 |  |  |
| 35 | 621 | 95.9 | 26.6 | 6.2 | 2.7 | 1.4 |  |  |
| 40 | 811 | 125 | 34.8 | 8.1 | 3.6 | 1.9 |  |  |
| 45 |  | 159 | 44.0 | 10.2 | 4.5 | 2.4 | 1.2 |  |
| 50 |  | 196 | 54.4 | 12.6 | 5.6 | 2.9 | 1.5 |  |
| 60 |  | 282 | 78.3 | 18.2 | 8.0 | 4.2 | 2.2 |  |
| 70 |  | 385 | 106 | 24.7 | 10.9 | 5.7 | 2.9 | 1.1 |
| 80 |  | 503 | 139 | 32.3 | 14.3 | 7.5 | 3.8 | 1.5 |
| 90 |  | 646 | 176 | 40.9 | 18.1 | 9.5 | 4.8 | 1.9 |
| 100 |  | 785 | 217 | 50.5 | 22.3 | 11.7 | 6.0 | 2.3 |
| 110 |  | 950 | 263 | 61.1 | 27.0 | 14.1 | 7.2 | 2.8 |
| 120 |  |  | 318 | 72.7 | 32.2 | 16.8 | 8.6 | 3.3 |
| 130 |  |  | 369 | 85.3 | 37.8 | 19.7 | 10.1 | 3.9 |
| 140 |  |  | 426 | 98.9 | 43.8 | 22.9 | 11.7 | 1.4 |
| 150 |  |  | 490 | 113 | 50.3 | 26.3 | 13.4 | 5.2 |
| 160 |  |  | 570 | 129 | 57.2 | 29.9 | 15.3 | 5.9 |
| 170 |  |  | 628 | 146 | 64.6 | 33.7 | 17.6 | 6.7 |
| 180 |  |  | 705 | 163 | 72.6 | 37.9 | 19.4 | 7.5 |
| 190 |  |  | 785 | 177 | 80.7 | 42.2 | 21.5 | 8.4 |
| 200 |  |  | 870 | 202 | 89.4 | 46.7 | 23.9 | 9.3 |
| 220 |  |  |  | 244 | 108 | 56.5 | 28.9 | 11.3 |
| 240 |  |  |  | 291 | 128 | 67.3 | 34.4 | 13.4 |
| 260 |  |  |  | 341 | 151 | 79.0 | 40.3 | 15.7 |
| 280 |  |  |  | 395 | 175 | 91.6 | 46.8 | 18.2 |
| 300 |  |  |  | 454 | 201 | 105 | 53.7 | 20.9 |

## Pressure Loss Through Pipe Fittings

This chart gives figures that are the air pressure flow losses through screw fittings expressed in the equivalent lengths of straight pipe of the same diameter. For example, a 2 " gate valve flow resistance would be the same as 1.3 foot of straight pipe.

| Pipe <br> Size | Gate | Long <br> Radius <br> NPT | Medium <br> Valve | Radius <br> Elbow |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Elbow* $^{* *}$ | Standard <br> Elbow*** | Angel <br> Valve | Close <br> Return <br> Bend | Tee <br> Thru <br> Side | Globe <br> Valve |  |  |  |
| $1 / 2$ | 0.31 | 0.41 | 0.52 | 0.84 | 1.1 | 1.3 | 1.7 | 2.5 |
| $3 / 4$ | 0.44 | 0.57 | 0.73 | 1.2 | 1.6 | 1.8 | 2.3 | 3.5 |
| 1 | 0.57 | 0.77 | 0.98 | 1.6 | 2.1 | 2.3 | 3.1 | 4.7 |
| $1-1 / 4$ | 0.82 | 1.1 | 1.4 | 2.2 | 2.9 | 3.3 | 4.4 | 6.5 |
| $1-1 / 2$ | 0.98 | 1.3 | 1.6 | 2.6 | 3.5 | 3.9 | 5.2 | 7.8 |
| 2 | 1.3 | 1.7 | 2.2 | 3.6 | 4.8 | 5.3 | 7.1 | 10.6 |
| $2-1 / 2$ | 1.6 | 2.2 | 2.8 | 4.4 | 5.9 | 6.6 | 8.7 | 13.1 |
| 3 | 2.1 | 3.0 | 3.6 | 5.7 | 7.7 | 8.5 | 11.4 | 17.1 |
| 4 | 3.0 | 3.9 | 5.0 | 7.9 | 10.7 | 11.8 | 15.8 | 23.7 |
| 5 | 3.9 | 5.1 | 6.5 | 10.4 | 13.9 | 15.5 | 20.7 | 31 |

* or run of Standard Tee
** or run of tee reduced in size by $25 \%$
*** or run of tee reduced in size by $50 \%$


## Friction of Air in Hose

Pressure Drop per 25 feet of hose. Factors are proportionate for longer or shorter lengths.

| Size | SCFM | 50 PSI | 60 PSI | 70 PSI | 80 PSI | 90 PSI | 100 PSI | 110 PSI |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1 / 2^{\prime}$ ID | 20 | 1.8 | 1.3 | 1 | 0.9 | 0.8 | 0.7 | 0.6 |
|  | 30 | 5 | 4 | 3.4 | 2.8 | 2.4 | 2.3 | 2 |
|  | 40 | 10.1 | 8.4 | 7 | 6 | 5.4 | 4.8 | 4.3 |
|  | 50 | 18.1 | 14.8 | 12.4 | 10.8 | 9.5 | 8.4 | 7.6 |
|  | 60 |  | 23.4 | 20 | 17.4 | 14.8 | 13.3 | 12 |
|  | 70 |  |  | 28.4 | 25.2 | 22 | 19.3 | 17.6 |
|  | 80 |  |  |  | 34.6 | 30.5 | 27.2 | 24.6 |
| $3 / 4$ ID | 20 | 0.4 | 0.3 | 0.2 | 0.2 | 0.2 | 0.2 | 0.1 |
|  | 30 | 0.8 | 0.6 | 0.5 | 0.5 | 0.4 | 0.4 | 0.3 |
|  | 40 | 1.5 | 1.2 | 0.9 | 0.8 | 0.7 | 0.6 | 0.5 |
|  | 50 | 2.4 | 1.9 | 1.5 | 1.3 | 1.1 | 1 | 0.9 |
|  | 60 | 3.5 | 2.8 | 2.3 | 1.9 | 1.6 | 1.4 | 1.3 |
|  | 70 | 4.4 | 3.8 | 3.2 | 2.8 | 2.3 | 2 | 1.8 |
|  | 80 | 6.5 | 5.2 | 4.2 | 3.6 | 3.1 | 2.7 | 2.4 |
|  | 90 | 8.5 | 6.8 | 5.5 | 4.7 | 4 | 3.5 | 3.1 |
|  | 100 | 11.4 | 8.6 | 7 | 5.8 | 5 | 4.4 | 3.9 |
|  | 110 | 14.2 | 11.2 | 8.8 | 7.2 | 6.2 | 5.4 | 4.9 |
| 1 1" ID | 30 | 0.2 | 0.2 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
|  | 40 | 0.3 | 0.3 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
|  | 50 | 0.5 | 0.4 | 0.4 | 0.3 | 0.3 | 0.2 | 0.2 |
|  | 60 | 0.8 | 0.6 | 0.5 | 0.5 | 0.4 | 0.4 | 0.3 |
|  | 70 | 1.1 | 0.8 | 0.7 | 0.7 | 0.6 | 0.5 | 0.4 |
|  | 80 | 1.5 | 1.2 | 1 | 0.8 | 0.7 | 0.6 | 0.5 |
|  | 90 | 2 | 1 | 1.3 | 1.1 | 0.9 | 0.8 | 0.7 |
|  | 100 | 2.6 | 2 | 1.6 | 1.4 | 1.2 | 1 | 0.9 |
|  | 110 | 3.5 | 2.6 | 2 | 1.7 | 1.4 | 1.2 | 1.1 |

## Vacuum Flow Trough Orifices

The chart below approximates flow that would be expected thorugh a practical orifice. Flows are $2 / 3$ of theoretical value obtained through a sharp edged orifice.

NOTE: Multiple smaller holes size grippers will work more efficently at higher vacuums.

Chart Valves are Air Flows in SCFM

| Orifice Dia., Inches | Degree of Vacuum Across |  |  |  | Orifice, Inches of Mercury (Hg) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 " | $4 "$ | $6 "$ | 8" | 10" | 12 " | $14 "$ | 18" | 24 " |
| 1/64 | 0.018 | 0.026 | 0.032 | 0.037 | 0.041 | 0.045 | 0.048 | 0.055 | 0.063 |
| 1/32 | 0.074 | 0.100 | 0.128 | 0.148 | 0.165 | 0.180 | 0.195 | 0.220 | 0.250 |
| 1/16 | 0.300 | 0.420 | 0.517 | 0.595 | 0.660 | 0.725 | 0.780 | 0.880 | 1.00 |
| 1/8 | 1.2 | 1.68 | 2.06 | 2.37 | 2.64 | 2.89 | 3.12 | 3.53 | 4.04 |
| 1/4 | 4.8 | 6.7 | 8.3 | 9.5 | 10.6 | 11.6 | 12.4 | 14.0 | 16.2 |
| 3/8 | 10.8 | 15.2 | 18.5 | 21.4 | 23.8 | 26.0 | 28.0 | 31.8 | 36.4 |
| 1/2 | 19.1 | 27.0 | 33.0 | 38.5 | 42.3 | 46.3 | 50.0 | 56.5 | 64.6 |
| 5/8 | 30.0 | 42.2 | 51.7 | 59.5 | 66.2 | 72.6 | 78.0 | 88.0 | 101 |
| 3/4 | 43.0 | 60.6 | 74.0 | 85.3 | 95.2 | 104 | 112 | 127 | 145 |
| 7/8 | 58.8 | 82.6 | 101 | 116 | 130 | 142 | 153 | 173 | 198 |
| 1 | 76.5 | 108 | 131 | 152 | 169 | 185 | 200 | 225 | 258 |

Decimal Equivalents
(of Fraction, Wire Gauge and Metric Sizes)

| Sizes | Decimal Inches | Sizes | Decimal Inches | Sizes | Decimal Inches | Sizes | Decimal Inches |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 107 | 0.0019 | . 7 mm | 0.0276 | 1.95 mm | 0.0768 | 3.7 mm | 0.1457 |
| 106 | 0.0023 | 70 | 0.0280 | 5/64 | 0.0781 | 26 | 0.1470 |
| 105 | 0.0027 | 69 | 0.0292 | 47 | 0.0785 | 3.75 mm | 0.1476 |
| 104 | 0.0031 | . 75 mm | 0.0295 | 2 mm | 0.0787 | 25 | 0.1495 |
| 103 | 0.0035 | 68 | 0.0310 | 2.05 mm | 0.0807 | 3.8 mm | 0.1496 |
| 102 | 0.0039 | 1/32 | 0.0312 | 46 | 0.0810 | 24 | 0.1520 |
| 101 | 0.0043 | . 8 mm | 0.0315 | 45 | 0.0820 | 3.9 mm | 0.1535 |
| 100 | 0.0047 | 67 | 0.0320 | 2.1 mm | 0.0827 | 23 | 0.1540 |
| 99 | 0.0051 | 66 | 0.0330 | 2.15 mm | 0.0846 | 5/32 | 0.1562 |
| 98 | 0.0055 | . 85 mm | 0.0335 | 44 | 0.0860 | 22 | 0.1570 |
| 97 | 0.0059 | 65 | 0.0350 | 2.2 mm | 0.0866 | 4 mm | 0.1575 |
| 96 | 0.0063 | . 9 mm | 0.0354 | 2.25 mm | 0.0886 | 21 | 0.1590 |
| 95 | 0.0067 | 64 | 0.0360 | 43 | 0.0890 | 20 | 0.1610 |
| 94 | 0.0071 | 63 | 0.0370 | 2.3 mm | 0.0906 | 4.1 mm | 0.1614 |
| 93 | 0.0075 | . 95 mm | 0.0374 | 2.35 mm | 0.0925 | 4.2 mm | 0.1654 |
| 92 | 0.0079 | 62 | 0.0380 | 42 | 0.0935 | 19 | 0.1660 |
| . 2 mm | 0.0079 | 61 | 0.0390 | 3/32 | 0.0938 | 4.25 mm | 0.1673 |
| 91 | 0.0083 | 1 mm | 0.0394 | 2.4 mm | 0.0945 | 4.3 mm | 0.1693 |
| 90 | 0.0087 | 60 | 0.0400 | 41 | 0.0960 | 18 | 0.1695 |
| . 22 mm | 0.0087 | 59 | 0.0410 | 2.45 mm | 0.0965 | 11/64 | 0.1719 |
| 89 | 0.0091 | 1.05 | 0.0413 | 40 | 0.0980 | 17 | 0.1730 |
| 88 | 0.0095 | 58 | 0.0420 | 2.5 mm | 0.0984 | 4.4 mm | 0.1732 |
| . 25 mm | 0.0098 | 57 | 0.0430 | 39 | 0.0995 | 16 | 0.1770 |
| 87 | 0.0100 | 1.1 mm | 0.0433 | 38 | 0.1015 | 4.5 mm | 0.1772 |
| 86 | 0.0105 | 1.15 mm | 0.0453 | 2.6 mm | 0.1024 | 15 | 0.1800 |
| 85 | 0.0110 | 56 | 0.0465 | 37 | 0.1040 | 4.6 mm | 0.1811 |
| . 28 mm | 0.0110 | 3/64 | 0.0469 | 2.7 mm | 0.1063 | 14 | 0.1820 |
| 84 | 0.0115 | 1.2 mm | 0.0472 | 36 | 0.1065 | 13 | 0.1850 |
| . 3 mm | 0.0118 | 1.25 mm | 0.0492 | 2.75 mm | 0.1083 | 4.7 mm | 0.1850 |
| 83 | 0.0120 | 1.3 mm | 0.0512 | 7/64 | 0.1094 | 4.75 mm | 0.1870 |
| 82 | 0.0125 | 55 | 0.0520 | 35 | 0.1100 | 3/16 | 0.1875 |
| . 32 mm | 0.0126 | 1.35 mm | 0.0531 | 2.8 mm | 0.1102 | 4.8 mm | 0.1890 |
| 81 | 0.0130 | 54 | 0.0550 | 34 | 0.1110 | 12 | 0.1890 |
| 80 | 0.0135 | 1.4 mm | 0.0551 | 33 | 0.1130 | 11 | 0.1910 |
| . 35 mm | 0.0138 | 1.45 mm | 0.0571 | 2.9 mm | 0.1142 | 4.9 mm | 0.1929 |
| 79 | 0.0145 | 1.5 mm | 0.0591 | 32 | 0.1160 | 10 | 0.1935 |
| 1/64 | 0.0156 | 53 | 0.0595 | 3 mm | 0.1181 | 9 | 0.1960 |
| . 4 mm | 0.0157 | 1.55 mm | 0.0610 | 31 | 0.1200 | 5 mm | 0.1969 |
| 78 | 0.0160 | 1/16 | 0.0625 | 3.1 mm | 0.1220 | 8 | 0.1990 |
| . 45 mm | 0.0177 | 1.6 mm | 0.0630 | 1/8 | 0.1250 | 5.1 mm | 0.2008 |
| 77 | 0.0180 | 52 | 0.0635 | 3.2 mm | 0.1260 | 7 | 0.2010 |
| . 5 mm | 0.0197 | 1.65 mm | 0.0650 | 3.25 mm | 0.1280 | 13/64 | 0.2031 |
| 76 | 0.0200 | 1.7 mm | 0.0669 | 30 | 0.1285 | 6 | 0.2040 |
| 75 | 0.0210 | 51 | 0.0670 | 3.3 mm | 0.1299 | 5.2 mm | 0.2047 |
| . 55 mm | 0.0217 | 1.75 mm | 0.0689 | 3.4 mm | 0.1339 | 5 | 0.2055 |
| 74 | 0.0225 | 50 | 0.0700 | 29 | 0.1360 | 5.25 mm | 0.2067 |
| . 6 mm | 0.0236 | 1.8 mm | 0.0709 | 3.5 mm | 0.1378 | 5.3 mm | 0.2087 |
| 73 | 0.0240 | 1.85 mm | 0.0728 | 28 | 0.1405 | 4 | 0.2090 |
| 72 | 0.0250 | 49 | 0.0730 | 9/64 | 0.1406 | 5.4 mm | 0.2126 |
| . 65 mm | 0.0256 | 1.9 mm | 0.0748 | 3.6 mm | 0.1417 | 3 | 0.2130 |
| 71 | 0.0260 | 48 | 0.0760 | 27 | 0.1440 | 5.5 mm | 0.2165 |


| Decimal Equivalents <br> (of Fraction, Wire Gauge and Metric Sizes) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sizes | Decimal Inches | Sizes | Decimal Inches | Sizes | Decimal Inches | Sizes | Decimal Inches |
| 7/32 | 0.2188 | 7.4mm | 0.2913 | V | 0.3770 | 21/32 | 0.6562 |
| 5.6 mm | 0.2205 | M | 0.2950 | 9.6 mm | 0.3780 | 17 mm | 0.6693 |
| 2 | 0.2211 | 7.5 mm | 0.2953 | 9.7 mm | 0.3819 | 43/64 | 0.6719 |
| 5.7 mm | 0.2244 | 19/64 | 0.2969 | 9.75 mm | 0.3839 | 11/16 | 0.6875 |
| 5.75 mm | 0.2264 | 7.6 mm | 0.2992 | 9.8 mm | 0.3858 | 17.5 mm | 0.6890 |
| 1 | 0.2280 | N | 0.3020 | W | 0.3860 | 45/64 | 0.7031 |
| 5.8 mm | 0.2283 | 7.7 mm | 0.3031 | 9.9 mm | 0.3898 | 18 mm | 0.7087 |
| 5.9 mm | 0.2323 | 7.75 mm | 0.3051 | 25/64 | 0.3906 | 23/32 | 0.7188 |
| A | 0.2340 | 7.8 mm | 0.3071 | 10 mm | 0.3937 | 18.5 mm | 0.7283 |
| 15/64 | 0.2344 | 7.9 mm | 0.3110 | $X$ | 0.3970 | 47/64 | 0.7344 |
| 6 mm | 0.2362 | 5/16 | 0.3125 | Y | 0.4040 | 19 mm | 0.7480 |
| B | 0.2380 | 8 mm | 0.3150 | 13/32 | 0.4062 | 3/4 | 0.7500 |
| 6.1 mm | 0.2402 | O | 0.3160 | Z | 0.4130 | 49/64 | 0.7656 |
| C | 0.2420 | 8.1 mm | 0.3189 | 10.5 mm | 0.4134 | 19.5 mm | 0.7677 |
| 6.2 mm | 0.2441 | 8.2 mm | 0.3228 | 27/64 | 0.4219 | 25/32 | 0.7812 |
| D | 0.2460 | P | 0.3230 | 11 mm | 0.4331 | 20 mm | 0.7874 |
| 6.25 mm | 0.2461 | 8.25 mm | 0.3248 | 7/16 | 0.4375 | 51/64 | 0.7969 |
| 6.3 mm | 0.2480 | 8.3 mm | 0.3268 | 11.5 mm | 0.4528 | 20.5 mm | 0.8071 |
| E | 0.2500 | 21/64 | 0.3281 | 29/64 | 0.4531 | 13/16 | 0.8125 |
| 1/4 | 0.2500 | 8.4 mm | 0.3307 | 15/32 | 0.4688 | 21 mm | 0.8268 |
| 6.4 mm | 0.2520 | Q | 0.3320 | 12 mm | 0.4724 | 53/64 | 0.8281 |
| 6.5 mm | 0.2559 | 8.5 mm | 0.3346 | 31/64 | 0.4844 | 27/32 | 0.8438 |
| F | 0.2570 | 8.6 mm | 0.3386 | 12.5 mm | 0.4921 | 21.5 mm | 0.8465 |
| 6.6 mm | 0.2598 | R | 0.3390 | 1/2 | 0.5000 | 55/64 | 0.8594 |
| G | 0.2610 | 8.7 mm | 0.3425 | 13 mm | 0.5118 | 22 mm | 0.8661 |
| 6.7 mm | 0.2638 | 11/32 | 0.3438 | 33/64 | 0.5156 | 7/8 | 0.8750 |
| 17/64 | 0.2656 | 8.75 mm | 0.3445 | 17/32 | 0.5312 | 22.5 mm | 0.8858 |
| 6.75 mm | 0.2657 | 8.8 mm | 0.3465 | 13.5 mm | 0.5315 | 57/64 | 0.8906 |
| H | 0.2660 | S | 0.3480 | 35/64 | 0.5469 | 23mm | 0.9055 |
| 6.8 mm | 0.2677 | 8.9 mm | 0.3504 | 14 mm | 0.5512 | 29/32 | 0.9062 |
| 6.9 mm | 0.2717 | 9 mm | 0.3543 | 9/16 | 0.5625 | 59/64 | 0.9219 |
| 1 | 0.2720 | T | 0.3580 | 14.5 mm | 0.5709 | 23.5 mm | 0.9252 |
| 7 mm | 0.2756 | 9.1 mm | 0.3583 | 37/64 | 0.5781 | 15/16 | 0.9375 |
| $J$ | 0.2770 | 23/64 | 0.3594 | 15 mm | 0.5906 | 24 mm | 0.9449 |
| 7.1 mm | 0.2795 | 9.2 mm | 0.3622 | 19/32 | 0.5938 | 61/64 | 0.9531 |
| K | 0.2810 | 9.25 mm | 0.3642 | 39/64 | 0.6094 | 24.5 mm | 0.9646 |
| 9/32 | 0.2812 | 9.3 mm | 0.3661 | 15.5 mm | 0.6102 | 31/32 | 0.9688 |
| 7.2 mm | 0.2835 | $\cup$ | 0.3680 | 5/8 | 0.6250 | 25mm | 0.9843 |
| 7.25 mm | 0.2854 | 9.4 mm | 0.3701 | 16 mm | 0.6299 | 63/64 | 0.9844 |
| 7.3 mm | 0.2874 | 9.5 mm | 0.3740 | 41/64 | 0.6406 | 1 | 1.0000 |
| L | 0.2900 | 3/8 | 0.3750 | 16.5 mm | 0.6496 |  |  |

# Conversions Between US Units (English) and SI Units (Metric) 

Quantity
Length
Pressure*
Vacuum**
Flow***
Force
Mass
Volume ${ }^{* * * *}$
Torque
Power
Frequency
Velocity

Temperature degrees Fahrenheit ( ${ }^{\circ} \mathrm{F}$ )
US Unit
inch (in.) pounds / sq. in. inches of mercury (in. Hg ) cubic feet per minute (cfm) pound (f) or lb. (f) pound ( m ) or lb. (m) gallon (US gallon) pounds (f) - inches (lbs (f) - in.) horsepower (HP) cycles per second (cps) feet per second (fps)

SI Unit
millimeter (mm)
bar
mm of mercury ( mm Hg )
cubic decimeters per sec (dm3/sec)
Newton (N)
kilogram (Kg)
liter (I)
degrees Celsius ( ${ }^{\circ} \mathrm{C}$ )
Newton-meters (Nm)
kilowatt (kw)
Hertz (Hz)
meter per second ( $\mathrm{m} / \mathrm{s}$ )

Coversion Factor
$1 \mathrm{in} .=25.4 \mathrm{~mm}$
$1 \mathrm{bar}=14.5 \mathrm{PSI}$
$1 \mathrm{Hg}=25.4 \mathrm{~mm} \mathrm{Hg}$
$2.12 \mathrm{cfm}=1 \mathrm{dm} 3 / \mathrm{sec}$
$1 \mathrm{lb}(\mathrm{f})=4.44 \mathrm{~N}$
$1 \mathrm{Kg}=2.2 \mathrm{lbs}$
1 US Gal = 3.71 ।
${ }^{\circ} \mathrm{C}=5 / 9\left({ }^{\circ} \mathrm{F}-32\right)$
$1 \mathrm{Nm}=8.88 \mathrm{lb}(\mathrm{f})$-in.
$1 \mathrm{kw}=1.34 \mathrm{HP}$
$1 \mathrm{~Hz}=1 \mathrm{cps}$
$1 \mathrm{~m} / \mathrm{s}=3.28 \mathrm{fps}$
*Above Atmospheric (PSI or Bar); **Below Atmospheric (Hg); ***Gas; (f) = force; (m) = mass

## Interchange Tables

How to Use: The following charts interchange units from the SI International Standard, the US system (or English System) and older metric systems. The left column is the basic SI unit. Equivalents are in the same line. To best use these charts, find the unit that is to be converted and move to the row with the " 1 " in it. Move in the same row to the unit you are changing the value to and multiply by that number to make the conversion.

## Torque

| Newton- <br> Meters | Kilopond- <br> Meters | Foot-Ibs | Inch-Ibs |
| :---: | :---: | :---: | :---: |
| 1 | $1.020 \times 10^{-1}$ | $7.376 \times 10^{-1}$ | 8.851 |
| 0.01 | 1 | 7.233 | 86.80 |
| 1.356 | $1.382 \times 10^{-1}$ | 1 | 12 |
| $1.130 \times 10^{-1}$ | $1.52 \times 10^{-2}$ | $8.333 \times 10^{-2}$ | 1 |

## Gravity Due to Acceleration

US System $(\mathrm{g})=32.2$ feet per sec. per sec. Metric System (g) $=105.5$ meters per sec. per sec

## Length

(Linear Measurement)

| Meter | Centimeter | Kilometer | Mile | Inch | Foot |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 100 | $1 \times 10^{4}$ | $6.214 \times 10^{-4}$ | 39.370 | 3.281 |
| 0.01 | 1 | $1 \times 10^{5}$ | $6.214 \times 10^{-6}$ | $3.937 \times 10^{-1}$ | $3.281 \times 10^{-2}$ |
| $1 \times 10^{-3}$ | 0.10 | $1 \times 10^{-6}$ | $6.214 \times 10^{-7}$ | $3.937 \times 10^{-2}$ | $3.281 \times 10^{-3}$ |
| $1 \times 10^{3}$ | $1 \times 10^{5}$ | 1 | $6.214 \times 10^{-7}$ | $3.937 \times 10^{4}$ | $3.281 \times 10^{3}$ |
| $1.609 \times 10^{3}$ | $1.609 \times 10^{5}$ | 1.609 | 1 | $6.336 \times 10^{4}$ | 5280 |
| $2.540 \times 10^{-2}$ | 2.540 | $2.540 \times 10^{-5}$ | $1.578 \times 10^{-5}$ | 1 | $8.333 \times 10^{-2}$ |
| $3.048 \times 10^{-1}$ | 30.479 | $3.048 \times 10^{-4}$ | $1.894 \times 10^{-4}$ | 12 | 1 |

$1 \mathrm{~mm}=0.001 \mathrm{~m}=0.10 \mathrm{~cm}=0.000001 \mathrm{~km}=0.03937 \mathrm{in}=0.003281 \mathrm{ft}$
AREA
(Square Measurement)

| Square Meter | Sq. Centimeter | Sq. Kilometer | Square Inch | Square Foot | Square Mile |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $1 \times 10^{4}$ | $1 \times 10^{6}$ | $1.550 \times 10^{3}$ | 10.764 | $3.861 \times 10^{-7}$ |
| $1 \times 10^{-3}$ | 1 | $1 \times 10^{-10}$ | $1.550 \times 10^{-1}$ | $1.076 \times 10^{-3}$ | $3.861 \times 10^{-11}$ |
| $1 \times 10^{-6}$ | $1 \times 10^{-2}$ | $1 \times 10^{-12}$ | $1.550 \times 10^{3}$ | $1.076 \times 10^{-5}$ | $3.861 \times 10^{-13}$ |
| $1 \times 10^{6}$ | $1 \times 10^{10}$ | 1 | $1.550 \times 10^{9}$ | $1.076 \times 10^{7}$ | $3.861 \times 10^{-1}$ |
| $6.452 \times 10^{-4}$ | 6.452 | $6.452 \times 10^{-10}$ | 1 | $6.944 \times 10^{-3}$ | $2.491 \times 10^{-10}$ |
| $9.290 \times 10^{-2}$ | $9.290 \times 10^{2}$ | $9.290 \times 10^{-8}$ | 144 | 1 | $3.587 \times 10^{-8}$ |
| $2.590 \times 10^{6}$ | $2.590 \times 10^{10}$ | 2.590 | $2.788 \times 10^{7}$ | $2.788 \times 10^{7}$ | 1 |

Volume (Cubic)

| Cubic Meter | Cu. Decimeter | Cu. Centimeter | US Gallon | Cu. Inch | Cubic Foot |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $1 \times 10^{3}$ | $1 \times 10^{6}$ | $2.642 \times 10^{2}$ | $6.102 \times 10^{4}$ | 35.314 |
| $1 \times 10^{-3}$ | 1 | $1 \times 10^{3}$ | $2.642 \times 10^{-1}$ | 61.024 | $3.531 \times 10^{-2}$ |
| $1 \times 10^{-6}$ | $1 \times 10^{-3}$ | 1 | $2.642 \times 10^{-4}$ | $6.102 \times 10^{2}$ | $3.531 \times 10^{-5}$ |
| $4.546 \times 10^{-3}$ | 4.546 | $4.546 \times 10^{3}$ | 1.200 | $2.774 \times 10^{2}$ | $1.605 \times 10^{-1}$ |
| $3.785 \times 10^{-3}$ | 3.785 | $3.785 \times 10^{3}$ | 1 | $2.310 \times 10^{2}$ | $1.337 \times 10^{-1}$ |
| $1.639 \times 10^{-5}$ | $1.639 \times 10^{-2}$ | 16.387 | $4.329 \times 10^{-3}$ | 1 | $5.787 \times 10^{-4}$ |
| $2.832 \times 10^{-2}$ | 28.317 | $2.832 \times 10^{4}$ | 7.481 | $1.728 \times 10^{3}$ | 1 |

1 imperial gallon $=1.2$ US gallon $=0.004546 \mathrm{cu}$. meter $=4.546$ liter $=4546 \mathrm{cu}$. centimeters
Force (Including Force due to Weight)

| Newton | Dyne | Kilopond | Metric Ton | US Ton | Pound |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $1 \times 10^{5}$ | $1.020 \times 10^{-1}$ | $1.020 \times 10^{-4}$ | $1.124 \times 10^{-4}$ | $2.248 \times 10^{-1}$ |
| $1 \times 10^{5}$ | 1 | $1.020 \times 10^{-6}$ | $1.020 \times 10^{-9}$ | $1.124 \times 10^{-9}$ | $2.248 \times 10^{-6}$ |
| 9.807 | $9.807 \times 10^{5}$ | 1 | $1 \times 10^{-3}$ | $1.102 \times 10^{-3}$ | 2.205 |
| $9.807 \times 10^{3}$ | $9.807 \times 10^{8}$ | 1000 | 1 | 1.102 | $2.205 \times 10^{3}$ |
| $9.964 \times 10^{3}$ | $9.964 \times 10^{8}$ | $1.016 \times 10^{2}$ | 1.016 | 1.120 | $2.240 \times 10^{3}$ |
| $8.896 \times 10^{3}$ | $8.896 \times 10^{8}$ | $9.072 \times 10^{2}$ | $9.072 \times 10^{-1}$ | 1 | 2000 |
| 4.448 | $4.448 \times 10^{5}$ | $4.536 \times 10^{-1}$ | $4.536 \times 10^{-4}$ | $5 \times 10^{-4}$ | 1 |

1 long ton $=9964$ Newtons $=1016$ Kiloponds $=1.016$ metric tons $=1.120$ US tons $=2240$ pounds
Mass (Not Weight)

| Kilogram | Gram | Metric Ton | Newton | Pound | US Ton |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1000 | $1 \times 10^{-3}$ | 9.807 | 2.205 | $1.102 \times 10^{-3}$ |
| $1 \times 10^{-3}$ | 1 | $1 \times 10^{-6}$ | $9.807 \times 10^{-3}$ | $2.205 \times 10^{-3}$ | $1.102 \times 10^{6}$ |
| $1 \times 10^{3}$ | $1 \times 10^{6}$ | 1 | $9.807 \times 10^{3}$ | $2.205 \times 10^{3}$ | 1.102 |
| $1.020 \times 10^{-1}$ | $1.020 \times 10^{2}$ | $1.020 \times 10^{-4}$ | 1 | $2.248 \times 10^{-4}$ | $1.120 \times 10^{-4}$ |
| $4.536 \times 10^{-1}$ | $4.536 \times 10^{2}$ | $4.536 \times 10^{-4}$ | 4.448 | 1 | $5 \times 10^{-4}$ |
| 14.594 | $1.459 \times 10^{4}$ | $1.459 \times 10^{-2}$ | $1.431 \times 10^{-2}$ | 32.170 | $1.609 \times 10^{-2}$ |
| $9.072 \times 10^{2}$ | $9.072 \times 10^{5}$ | $9.072 \times 10^{-1}$ | $8.896 \times 10^{3}$ | 2000 | 1 |

Unit Pressure (Either Fluid or Mechanical)

| Bar | Newton $/ \mathrm{m}^{2}$ <br> (Pascal) | Kilopond $/ \mathrm{m}^{2}$ | Atmosphere | Pounds/Ft ${ }^{2}$ | Pounds/Inch <br> (PSI) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $1 \times 10^{-5}$ | 1 | $1.020 \times 10^{-1}$ | $9.869 \times 10^{6}$ | $2.088 \times 10^{-2}$ | $1.45 \times 10^{-4}$ |
| 1 | $1 \times 10^{6}$ | $1.020 \times 10^{4}$ | $9.869 \times 10^{-1}$ | $2.088 \times 10^{3}$ | 14.5 |
| $9.807 \times 10^{-5}$ | 9.807 | 1 | $9.678 \times 10^{-5}$ | $2.048 \times 10^{-1}$ | $1.422 \times 10^{-3}$ |
| $9.807 \times 10^{-1}$ | $9.807 \times 10^{4}$ | $1 \times 10^{4}$ | $9.678 \times 10^{-1}$ | $2.048 \times 10^{3}$ | 14.220 |
| 1.013 | $1.013 \times 10^{5}$ | $1.033 \times 10^{4}$ | 1 | $2.116 \times 10^{3}$ | 14.693 |
| $4.789 \times 10^{-4}$ | 47.893 | 4.884 | $4.726 \times 10^{-4}$ | 1 | $6.944 \times 10^{-3}$ |
| $6.897 \times 10^{-2}$ | $6.897 \times 10^{3}$ | $7.033 \times 10^{2}$ | $6.806 \times 10^{-2}$ | $1.440 \times 10^{2}$ | 1 |

1 kiloponds $/ \mathrm{sq} \mathrm{cm}=0.9807 \mathrm{bar}=98070$ Pascal $=0.9678 \mathrm{atmos}=2048 \mathrm{lbs} / \mathrm{sq} \mathrm{ft}=14.22 \mathrm{lbs} / \mathrm{sq} \mathrm{in}$

## Velocity

| Meters / Second | Kilometers / Hour | Miles / Hour | Feet / Minute | Feet / Second | Inches / Minute |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 3.6 | 2.237 | $1.968 \times 10^{2}$ | 3.281 | $2.362 \times 10^{3}$ |
| $1 \times 10^{-1}$ | $1 \times 10^{-4}$ | $6.214 \times 10^{-5}$ | $5.468 \times 10^{-3}$ | $9.113 \times 10^{-5}$ | $6.562 \times 10^{-2}$ |
| $2.778 \times 10^{-1}$ | 1 | $6.214 \times 10^{-1}$ | $5.468 \times 10^{-1}$ | $9.113 \times 10^{-1}$ | $6.562 \times 10^{2}$ |
| $4.470 \times 10^{-1}$ | 1.609 | 1 | 88 | 1.467 | $1.056 \times 10^{3}$ |
| $5.080 \times 10^{-3}$ | $1.829 \times 10^{-2}$ | $1.136 \times 10^{-2}$ | 1 | $1.667 \times 10^{-2}$ | 12 |
| $3.048 \times 10^{-1}$ | 1.097 | $6.818 \times 10^{-1}$ | 60 | 1 | $7.2 \times 10^{2}$ |
| $4.233 \times 10^{-4}$ | $1.524 \times 10^{-3}$ | $9.470 \times 10^{-4}$ | $8.333 \times 10^{-2}$ | $1.389 \times 10^{-3}$ | 1 |

[^0]
[^0]:    1 decimeter $/$ second $=0.1$ meters $/$ second $=0.005468$ feet $/$ minute $=0.06562$ inches $/$ minute

